

Figure 1.—Effect of rate and duration of flushing with nitrogen on induction period for ammonium nitrate containing sodium chloride at a mole ratio of 0.05 at 185°.

to decomposition under steady-state conditions only. The postulated intermediates, however, are produced during the preceding induction period which is the subject of the present study.

Qualitative observations on the induction period by previous workers have established that ammonium nitrate-chloride melts develop acidity and evolve traces of  $\text{HNO}_3$ ,  $\text{HCl}$ , and  $\text{Cl}_2$  along with the major products of the decomposition,  $\text{N}_2$ ,  $\text{N}_2\text{O}$ , and  $\text{H}_2\text{O}$ , during this period. It has also been demonstrated that addition to the melt of acidic species or of  $\text{Cl}_2$  decreases the induction period, whereas basic species increase it. Guiochon<sup>3</sup> has attempted a more quantitative study of the induction period but his values include the time required for melting and thermal equilibration. In the present work, a technique of flushing with inert gas at reaction temperature has been used to reduce the reaction rate to a negligible value. This provides an unambiguous zero time for the measurements. The induction period is defined as the time from cessation of flushing to the rate maximum,  $R_m$  (see Figure 1 of ref. 1). The results are highly reproducible and can be interpreted on the basis of acid autocatalysis.

### Experimental

**Apparatus.**—The reactor was similar to those previously described<sup>1,2,4</sup> except that the top was furnished with a ground joint through which either a thermometer or a flushing tube

could be inserted. The latter consisted of 4-mm. tubing with a 2-mm. orifice at the end. The reactor was immersed in a  $\text{LiNO}_3$ - $\text{KNO}_3$  eutectic fused-salt bath regulated at  $185.0 \pm 0.1^\circ$ . Temperatures were read with a mercury thermometer calibrated against an ASTM precision grade standard. Reaction rates were measured with a soap-film flow meter following a KOH trap.<sup>1,4</sup> The chemicals were reagent grade and the flushing gas was dry  $\text{N}_2$ .

**Procedure.**—The heated reactor was charged with 6 g. of  $\text{NH}_4\text{NO}_3$  and the necessary  $\text{NaCl}$  to bring the mole ratio either to 0.05 or to 0.10. The preheated flushing tube was inserted after 5 min. and flushing was begun after another 5 min. At the termination of flushing ( $t_0$ ), an electric timer was started for measurement of the induction period, the flushing tube was replaced with a preheated thermometer, and rate measurements were taken at intervals for a suitable period of time. Some runs were also made in which the chloride was added at the termination of flushing. Values of the induction period were obtained from a plot of rate against time. They were reproducible to  $\pm 1\%$ . All values given are averages of three or more replicates.

At the requisite time, the reactor was chilled by immersing in cold water. Volhard chloride analyses and pH measurements using a Beckman Model G pH meter, standardized at pH 2.00, were carried out on aliquots of a 100-ml. aqueous solution of the reactor contents. The pH measurements were reproducible to within a few hundredths of a unit.

### Results

Data for the 0.05 mole ratio melts in which chloride was added before flushing are shown in Figure 1. The results for the 0.10 mole ratio melts were similar. The induction period for unflushed melts ( $t_f = 0$ ) was of the order of 75–100 min., depending on the chloride concentration, but was not investigated in detail because experience showed that the reproducibility of the measurements became poorer for shorter flushing times. Furthermore, the label values of the pH of different lots of reagent ammonium nitrate varied from 4.9 to 5.4 and the actual pH values changed on standing.

The induction period at first decreases rapidly with increasing  $t_f$  at constant  $R_f$  and then, except for  $R_f = 10$  cc./min., attains a constant value ( $\pm 0.1$  min.) for  $t_f$  values ranging from about 20 to as long as 60 min. These constant induction period values which are characteristic of each combination of melt composition and flushing rate, and are independent of flushing time over the above range, are assigned the symbol  $t_i$ . Numerical values are given in Table I. The induction period values for the cases where chloride was added after flushing were also independent of  $t_f$  in the range 20–60 min. and are included in Table I.

TABLE I  
INDUCTION PERIODS AT 185°

$R_f$ , cc./ min.	$t_i$ , min.			
	$\text{NaCl}/\text{NH}_4\text{NO}_3 = 0.05$		$\text{NaCl}/\text{NH}_4\text{NO}_3 = 0.10$	
	A <sup>a</sup>	B <sup>b</sup>	A <sup>a</sup>	B <sup>b</sup>
75	34.9	35.1	33.0	30.6
50	32.9	34.7	32.4	30.1
25	29.8	34.6	28.0	30.0

<sup>a</sup> A = NaCl added before flushing. <sup>b</sup> B = NaCl added after flushing.

Results of pH measurements are given in Table II. The values for pure ammonium nitrate melts containing no chloride at  $t_0$ , *i.e.*, at the termination of flushing,

(3) G. Guiochon, *Ann. Chim. (Paris)*, **5**, 295 (1960).

(4) A. G. Keenan and B. Dimitriades, *Trans. Faraday Soc.*, **57**, 1019 (1961).

TABLE II  
 pH OF STANDARD AQUEOUS SOLUTIONS

$R_f$ , cc./ min.	$t_f$ , min.	pH							
		NH <sub>4</sub> NO <sub>3</sub>		NaCl/NH <sub>4</sub> NO <sub>3</sub> = 0.05				NaCl/NH <sub>4</sub> NO <sub>3</sub> = 0.10	
		$t_0$	$t_0$	$t_1$	$t_1 + 15$	$t_0$	$t_1$	$t_1 + 15$	
75	20	3.51	3.60			3.71			
	40	3.53	3.62	2.27	2.31	3.72	2.26	2.29	
	60	3.52	3.59			3.70			
50	20	3.53	3.50			3.65			
	40	3.52	3.46	2.32	2.31	3.63	2.32	2.30	
	60	3.54	3.49			3.63			
25	30	3.52	3.45			3.53			
	40	3.52	3.39	2.28	2.29	3.47	2.29	2.30	
	60	3.52	3.29			3.37			

are constant at  $3.52 \pm 0.01$  for all  $R_f$  and  $t_f$  values. In the case of the chloride-containing melts, however, the pH shows significant variations greater than the reproducibility of the measurements. The chloride analyses indicated that the loss of chloride during flushing was negligible.

### Discussion

The precision of the  $t_i$  measurements and the constancy of the values after 15–20 min. flushing for  $R_f$  greater than 10 cc./min. indicates the establishment of a reproducible melt composition in each case. The flushing procedure, therefore, appears satisfactory for initiating accurate induction period measurements in systems of this type. Furthermore, since the flushing is carried out at reaction temperature, the  $t_i$  values do not include the time required for melting and for thermal equilibration as in previous work.

In Figure 1, the initial rapid decrease of induction period with increasing  $t_f$  indicates that flushing removes a volatile inhibitor. The relative positions of the initial portions of the curves show that the more rapid the flushing, the more rapid the removal of inhibitor and the sooner steady-state conditions are reached. When the induction period becomes constant, however, the curves have all crossed and a higher  $R_f$  now corresponds to a longer  $t_i$ . Turning to the pH values of the chloride-containing melts in the  $t_0$  columns of Table II, it is seen that flushing has increased the acidity of the melts relative to values in the range 4.9–5.4 which, as mentioned earlier, are characteristic of unflushed melts. No change in acidity on further flushing occurs in the region in which  $t_i$  is constant, *i.e.*, a true steady-state condition exists. The higher this steady-state acidity, the shorter is  $t_i$ , and the lower was the flushing rate which produced it.

The above observations together with the known chemistry of these systems indicate that the following mechanisms are operating during the induction period. Initially NH<sub>3</sub> is preferentially volatilized by flushing. The resulting increase in melt acidity has two effects. First, the dissociation of NH<sub>4</sub>NO<sub>3</sub> is repressed and the rate of NH<sub>3</sub> removal decreased. Secondly, the increased acidity catalytically initiates the decomposition reaction which increases the acidity further. Volatilization of acid therefore increases according to the usual

Henry's law concept. A steady state is reached when NH<sub>3</sub> and acid are removed in such a ratio that the melt acidity remains constant. The rate of volatile acid removal by flushing equals the sum of the rates of acid generation by slow decomposition and of acid release from the NH<sub>4</sub>NO<sub>3</sub> due to the residual rate of NH<sub>3</sub> volatilization. When flushing is terminated, the acid autocatalytic reaction gradually builds up the acidity and the reaction rate increases until a new steady state is reached. The evolution of product gases N<sub>2</sub>, N<sub>2</sub>O, and H<sub>2</sub>O now performs the flushing function and maintains the acidity constant at a higher level, as shown by the entries in the  $t_i$  and  $t_i + 15$  columns of Table II. The time required for this readjustment of acidity levels is the explanation of the induction period.

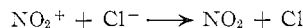
Further study of correlations among the data, some of which appear anomalous at first, serves to corroborate the picture developed so far. The increase in  $t_i$  with increase in  $R_f$  for a given initial chloride concentration is explained on the basis that increase of  $R_f$  lowers the steady-state concentration of volatile acids and a longer period of time will be required to generate the acidity necessary for termination of the induction period (columns A in Table I). This view is substantiated by the fact that a constant induction period is not attained at an  $R_f$  as low as 10 cc./min. (Figure 1). The rate of removal of volatile acid at this low  $R_f$  does not balance the rate of generation through decomposition. At the next higher rate,  $R_f = 25$  cc./min., a constant  $t_i$  is attained, but it will be noted that in the  $t_0$  columns of Table II there is a small but consistent increase in acidity in contrast to the very constant values for  $R_f = 50$  and 75. Apparently this is a borderline case where the  $R_f$  is not quite sufficient to maintain the acidity constant but the effect is not large enough to show up in the  $t_i$  measurements.

The pH data for pure ammonium nitrate in Table II show that these melts also develop a constant acidity on flushing. In the absence of the chloride catalyst, however, this acidity is not high enough to initiate decomposition at this temperature and these melts show no induction period. In contrast to the chloride-containing melts, the acidity is rigorously independent of  $R_f$  as well as of  $t_f$  since the acid autocatalytic reaction

is not operating in the absence of chloride. The volatile acid in pure ammonium nitrate melts is  $\text{HNO}_3$ . In the chloride-containing melts, volatilization of  $\text{HCl}$  and of  $\text{Cl}_2$  also occurs, the rate depending on the respective Henry's law coefficients and on the melt concentrations. Although the loss of chloride was not detectable analytically, it may be sufficient to account for the fact that in Table II the pH of the 0.10 mole ratio melts at the termination of flushing ( $t_0$ ) is uniformly about 0.1 unit higher at each  $t_f$  than for the 0.05 melts.

The  $t_f$  values in the *B* columns of Table I are independent of  $R_f$  within experimental error, in marked contrast to the data in the *A* columns. When chloride is added to the melt after flushing, it is added to a melt of constant acidity, irrespective of  $R_f$ , since the data in Table II show that the acidity produced by flushing pure ammonium nitrate is independent of  $R_f$  and  $t_f$ . The dependence of the induction period on both acidity and chloride concentration undoubtedly accounts for the inability of Guiochon<sup>3</sup> to find any consistent variation of his induction periods with chloride concentration alone.

The complete mechanism for decomposition under steady-state conditions<sup>1</sup> is rather complex, but the important features for the present discussion may be summarized very briefly as follows. The key step is the reaction



where the  $\text{NO}_2^+$  is generated by the autoprotolysis of the  $\text{HNO}_3$  resulting from the dissociation of the am-

monium nitrate. The radicals  $\text{NO}_2$  and  $\text{Cl}$  then initiate a set of cage reactions which lead to  $\text{N}_2\text{O}$  through nitramide as a precursor, and to  $\text{N}_2$  by two paths with nitrosamine and chloramine as precursors. The mechanism therefore requires an initial excess of acidity to allow formation of  $\text{NO}_2^+$ .

It has been shown subsequently<sup>5</sup> that the mass balance is such that the  $\text{N}_2$ -producing reactions generate more acidity than they consume. The reaction is therefore potentially acid autocatalytic, except that volatilization of acid may produce a steady state at various levels of acidity depending on the conditions. In fact, the observed unsymmetrical bell-shaped rate curve has further been shown<sup>5</sup> to be characteristic of a second-order autocatalytic reaction in which the concentration of the reactants attains a constant value after the rate maximum. In Table II, the pH values at  $t_f$ , which represents the rate maximum  $R_m$ , and at  $t_f + 15$  min., which is well into the region of spontaneous steady-state decomposition, are all constant at  $2.30 \pm 0.02$  pH units irrespective of prior  $R_f$  or  $t_f$ . The present data, therefore, in addition to providing a mechanistic explanation for the induction period, also confirm the arguments used earlier<sup>1</sup> to justify an important assumption in the mechanism, namely, that the freely decomposing melts spontaneously develop a constant steady-state acidity.

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(5) C. I. Colvin, Ph.D. Thesis, University of Miami, 1963.

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## The Niobium Iodides. Characterization of Niobium(IV) Iodide, Niobium(III) Iodide, and Triniobium Octaiodide<sup>1</sup>

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The condensed niobium–niobium(V) iodide system contains three intermediate phases,  $\text{NbI}_4$ ,  $\text{NbI}_3$ , and  $\text{Nb}_3\text{I}_8$ , all qualitatively diamagnetic at room temperature. Niobium tetraiodide is evidently trimorphic. The weakly endothermic  $\alpha \rightarrow \beta$  transition observed at *ca.*  $348^\circ$  only on heating is without effect in the powder pattern data. A more substantial  $\beta \rightarrow \gamma$  transition occurs at  $417^\circ$ , and  $\gamma\text{-NbI}_4$  melts incongruently at  $503^\circ$  to form an iodide-rich liquid and solid  $\text{Nb}_3\text{I}_8$ . Niobium(III) iodide may be obtained by thermal decomposition of  $\text{NbI}_4$ , as a sublimate from mixtures with  $\text{Nb}_3\text{I}_8$ , or as the initial product of oxidation of excess metal. The phase is apparently not an equilibrium compound in the system since it decomposes slowly and irreversibly at about  $513^\circ$  into iodide-rich liquid and  $\text{Nb}_3\text{I}_8$ . The phase in equilibrium with the metal is  $\text{Nb}_3\text{I}_8$  ( $\text{NbI}_{2.67=0.02}$ ), which may also be obtained by thermal decomposition of higher iodides or as the phase transported from mixtures with metal. The two lower niobium iodides show only a limited correspondence with those reported in the niobium chloride and bromide and tantalum iodide systems.

### Introduction

Although several investigators<sup>2–7</sup> have reported syn-

thesis of niobium(V) iodide samples of varying purity,

(1) Work was performed in the Ames Laboratory of the U. S. Atomic Commission.

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